







Conceptual model of the South basin

- A simplified two-step scenario to explain sulphate rise in the flooded mine:
 - During the mining: pyrite oxidation + neutralization by carbonates
 → gypsum at the surface of rock fractures
 - During the flooding: dissolution of the gypsum
 → high sulphate concentration in water
- An experimental solid sulphate precipitation-dissolution reaction rate :

$$\frac{d[SO_4^{2^-}]}{dt} = k_{pcp}.m(t)^2.(K_{eq} - [SO_4^{2^-}])$$

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Model development: cartographic analysis



Model development: finding out an Epanet equivalent of the functional unit





Calibrating model : calculating the recharge rate of each functional unit

- Total recharge rate (overflow + pumpings) of the flooded mine is modelled using the TEMPO computer code, which is based on signal-processing methods:
- Calculation of the impulse response of the system...
- ...allow to ajust the observed total recharge rate...
 ...and to simulate future recharge by

stochastic methods



Pas échant.=1.00 j (base=1.00 j)

 Then, each functional unit receives a part of this total recharge, proportionaly to its relative area

Calibrating model: adjusting chemical parameters

 In a previous work, we added our experimental solid sulphate dissolution-precipitation reaction rate to the Epanet water-quality solver:

$$\frac{d[SO_4^{2^-}]}{dt} = k_{pcp} n(t)^2 (K_{eq} - [SO_4^{2^-}])$$

- To calibrate the model, we needed to adjust two global parameters:
 - the global apparent kinetic precipitation constant
 the global initial available mass of solid sulphate
- We also fixed an initial sulphate concentration in water for each tank and pipe

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Conclusion

- The numerical model gives good agreement between calculated and observed sulphate concentrations... but for few available monitoring points.
- Our hydrogeochemical conceptual model as well as our numerical approach seem to be relevant for the South basin...
- ...but need to be tested for Centre and North basin modelling.

